# **Effects of annealing on magnetic properties of Fe78B13Si9**

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We have annealed amorphous Fe<sub>78</sub>B<sub>13</sub>Si<sub>9</sub> samples at temperatures  $T_a = 355$  to 460°C for time  $t_{\rm a}$  = 10 to 60 min, in an atmosphere with purging of nitrogen gas. After thermal treatment, we examined the hysteresis loop, DSC curve, and the X-ray diffractogram of each sample. The coercivity  $H_c$ , the peak induction  $B_{\text{max}}$ , and the loss  $W_h$  were analysed to study the affects of annealing. Stress-relief and partial crystallization are two important parameters in determining optimal annealing conditions.

## **1. Introduction**

Metallic glasses obtained by the melt-spinning method are useful in many industrial applications. In particular, the commercialized  $Fe_{78}B_{13}Si_9$  glass (2605S2) is characterized by high magnetization  $M_s \simeq 1.5$  T and high magnetostriction  $\lambda_s \simeq 3 \times 10^{-5}$  from other glasses [1]. Large residual stresses formed during casting, mean that proper annealing is usually needed for this kind of glass to improve its magnetic properties such as peak induction  $B_{\text{max}}$ , coercivity  $H_c$ , and the loss  $W_h$ . However, since the Fe<sub>78</sub>B<sub>13</sub>Si<sub>9</sub> glass is in a metastable state, the annealing conditions including the annealing temperature  $T_a$ , and the annealing time  $t<sub>a</sub>$  should be properly defined so that no excessive crystallization occurs. Generally, crystallization is deleterious except for some applications in the high frequency range [2]. Also, as discussed in this paper, by annealing the  $Fe_{78}B_{13}Si_9$  glass in a protected atmosphere, partial crystallization would have started for  $T_a > 400^{\circ}$ C, irrespective of the annealing time chosen. In this paper, the affects of annealing on low frequency (60 Hz) properties will mainly be discussed.

## **2. Experimental procedures**

The Fe<sub>78</sub>B<sub>13</sub>Si<sub>9</sub> glass was purchased from the Allied corporation, USA. Our samples were cut from a master ribbon with dimensions of  $1.5 \times 150 \times 0.022$  mm<sup>3</sup>. Depending on the annealing conditions as shown in Table I, we have labelled the samples from 0 to 24. The heat treatment was performed in the atmosphere with purging of purified nitrogen gas. The flow rate was set at  $50 \text{ ml} \text{ min}^{-1}$ . The heating rate was kept around  $5^{\circ}$  C min<sup>-1</sup>. The sample is set in a bed made of stainless steel. By automatic temperature control,  $T_a$  was stabilized to within  $1^{\circ}$ C of the programmed temperature. After a preset annealing time  $t_{\rm a}$ , the sample was immediately extracted from the furnace, and cooled rapidly to room temperature [3].

After various annealings, samples 0 to 24 were

obtained for the hysteresis measurements at 60Hz. *ABH* loop tracer was set up for this purpose [4]. The maximum external field used was 60e. The data of peak induction, coercivity, and loss were gathered together and analysed by an IBM PC.

For auxiliary measurements, we have cut small pieces of 0 to 24 samples and run their DSC data in a DuPont 9900 system. The heating rate used was also set at  $5^{\circ}$ Cmin<sup>-1</sup>. Sample 2 to 4, 13, and 24  $(T_a > 385$ °C) were analysed with CuK $\alpha$  X-ray to determine the crystallized phase [5]. To further determine the thickness of the crystallized layer, each sample was etched about 1  $\mu$ m each side in a polishing solution of 30% HNO<sub>3</sub>, 10% H<sub>2</sub>SO<sub>4</sub>, 10% H<sub>3</sub>PO<sub>4</sub>,  $50\% \text{ CH}_3\text{COOH}$ , and exposed to the same X-ray for comparison. The thickness of the sample was determined by the density and mass method [6].

### **3. Results and discussion**

All the samples, except sample 1, show the characteristics of two-peak DSC curves. As in Fig. 1, the first crystallization peak appears at  $T_{x1} = 527.9^{\circ}$ C, and the second peak at  $T_{x2} = 542.1^{\circ}$  C. However, it is clear that for sample 1, the first peak has disappeared. Hence, although it is difficult to associate the first peak totally with the  $\alpha$ -ion crystallization, we may still conclude that for  $T_a = 460^{\circ}$ C sample 1 has crystallized substantially. This sets the upper limit of any useful annealing condition for  $Fe_{78}B_{13}Si_9$  glass.

To make certain of the crystallized phase and its distributed thickness in the annealed  $Fe_{78}B_{13}Si_9$  glass, we scanned several samples (as discussed in Section 2) in a X-ray diffractometer. Sample 24 ( $T_a = 385$ °C) did not show any obvious pattern of crystallization. However, all the rest showed the similar results to that of sample 13, shown in Fig. 2. For the unetched sample 13, the observed peak at  $2\theta \simeq 44.8^\circ$  is associated with  $\alpha$ -Fe or  $\alpha$ -(FeSi) [5]. After etching, the peak disappeared. This may indicate that partial

TABLE I Annealing conditions of samples

Sample	$T_{\rm a}$ (°C)	$t_a$ (min)	
$\bf{0}$	as-cast		
$\mathbf{I}$	460	10	
	445	10	
$\frac{2}{3}$	430	10	
$\overline{4}$	415	10	
5	415	20	
$\boldsymbol{6}$	415	30	
$\boldsymbol{7}$	430	20	
8	400	20	
9	400	30	
10	400	40	
11	385	60	
12	385	40	
13	400	10	
14	385	30	
15	385	20	
16	370	60	
17	370	40	
18	370	30	
19	370	20	
20	355	60	
21	355	20	
22	355	40	
23	355	30	
24	385	10	

crystallization has occurred in surface layers of about 0.5 to 1  $\mu$ m thick in these samples. Although we did not check other samples, it is believed that for a longer annealing time, the degree of crystallization or the layer thickness increases further. These affects will be seen and discussed in the context of the magnetic properties.

Fig. 3 shows the coercivities  $H_c$  of samples 0 to 24 measured from the maximum field to the 10e *BH*  loop. For the as-cast sample  $H_e \simeq 0.17$  Oe.  $H_e$  reaches a minimum ( $\simeq 0.075 \,\text{Oe}$ ) for the batch of  $T_a = 370^{\circ}$ C samples. Hence, many of the stresses have been removed in samples for these kinds of annealing. By raising  $T_a$  further,  $H_c$  increases. Moreover, as  $T_a > 400^{\circ}$ C,  $H_c$  increases distinctly with annealing time  $t_a$  even for a relatively short anneal which indicates that crystallites enhance pinning. To explore more of the magnetic properties, we plotted the peak induction  $B_{\text{max}}$  of each sample for the 60e *BH* loop as in Fig. 4. The horizontal axis of Fig. 4 was so placed that both  $T_a$  and  $t_a$  increase from left to right. It is then obvious that by annealing at  $T_a =$ 355°C and  $t_a = 40$  min,  $B_{\text{max}}$  reaches the highest



*Figure 1* Differential scanning calorimeter recordings of samples 14 and I.



*Figure 2* X-ray diffractograms of sample 13 (unetched) and I3 (etched) samples.

value of 1.47T. This also shows that  $T_a = 355$  to 370~ annealing is sufficient for stress relief in the sample. Continuing to raise  $T_a$  and to prolong  $t_a$  will result in a slight decrease of  $B_{\text{max}}$  until  $T_a \simeq 400$ °C. For  $T_a > 400^\circ \text{C}$ , partial crystallization affects  $B_{\text{max}}$  in two ways: (a) a tensile stress in the crystalline surface layer will force magnetization to lie in the surface plane, and  $\alpha$ -Fe crystallites will enhance the magnetization (per unit volume), (b) a compressive stress in the amorphous layer will tilt the magnetization out of the plane of layer [7]. Hence, by combining these two affects, it is not difficult to explain the observed decreasing and then increasing behaviours of  $B_{\text{max}}$  for  $T_{\rm a}$  > 400°C.

Finally, for discussion of loss  $W<sub>h</sub>$ , Fig. 5 shows  $W<sub>h</sub>$ at  $B_{\text{max}} = 1.2$  T for all samples. The horizontal axis is similar to that of Fig. 4. The loss in the as-cast sample (0) is too large  $(\approx 1.5 \text{W kg}^{-1})$  to be shown in the figure. From Fig. 5, it is clear that there exists a minimum of  $W<sub>h</sub>$  for all the thermally treated samples. This minimum lies closely in the batch of  $T_a = 385$ °C,  $t_a > 20$  min samples. Thus, to obtain an optimal sample from annealing for low frequency uses, it is better to release the stress in the sample completely rather than to partially crystallize it.

#### **4. Conclusions**

We have discussed the affects of annealing ( $T_a = 355$ ) to 460°C, and  $t_a = 10$  to 60 min) on the magnetic properties of  $Fe_{78}B_{13}Si_9$ . For  $T_a$  in the range of 370 to 385 $^{\circ}$ C, and  $t_a$  in the range of 20 to 60 min, it is sufficient to stress-relieve the sample, and to optimize its magnetic properties. To anneal at higher  $T<sub>s</sub>$  or longer  $t_a$  (T<sub>a</sub> > 400°C) will crystallize the sample. We have



*Figure 3* The coercive force  $H_c$  ( $H_{\text{max}} = 1$  Oe) of samples 0 to 24. ( $\Box$ 355°C,  $\blacksquare$  370°C,  $\triangledown$  385°C,  $\triangle$  390°C,  $\times$  400°C,  $\blacklozenge$  410°C, + 415° C,  $\times$  430° C, Y 445° C,  $\Diamond$  460° C,  $\Diamond$  cast).



*Figure 4* The peak induction  $B_{\text{max}}$  ( $H_{\text{max}} = 6$  Oe) of samples 0 to 24.

found the crystallized phase to be  $\alpha$ -Fe related. Our **conclusions have been based on the condition of anneals in a protecting atmosphere. If the oxidizing environment during anneals had been changed, the result would have been different. It is still not clear which mechanism triggers the surface crystallization, and therefore changes the upper limit for the optimal anneal [8]. Evidence has shown that by annealing**   $Fe_{78}B_{13}Si_9$  in vacuum, the optimal condition may be **shifted to 400 to 410~ [9].** 

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*Figure 5* The loss  $W_h$  at  $B_{\text{max}} = 1.2$  T for samples 0 to 24.

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